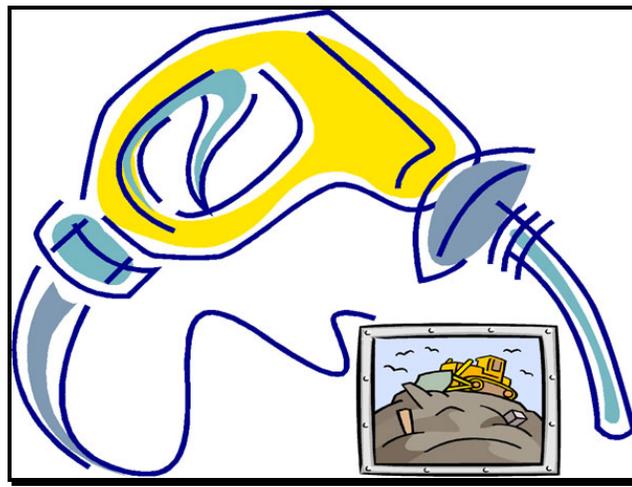


Detailed California-Modified GREET Pathway for Compressed Natural Gas (CNG) from Landfill Gas



Stationary Source Division
Release Date: February 28, 2009
Version: 2.1

The Staff of the Air Resources Boards developed this preliminary draft version as part of the Low Carbon Fuel Standard regulatory process.

The ARB acknowledges contributions from the California Energy Commission, TIAX, and Life Cycle Associates during the development of this document.

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These comments will be compiled, reviewed, and posted to the LCFS website in a timely manner.

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SUMMARY

CA-GREET Model Pathway for CNG from Landfill Gas

Well-To-Tank (WTT) Life Cycle Analysis of a fuel pathway considers all fuel production steps from feedstock recovery to finished fuel. Tank-To-Wheel (TTW) analysis includes actual combustion of fuel in a motor vehicle for motive power. Together, WTT and TTW analysis are combined to provide a total Well-To-Wheel (WTW) analysis.

A Life Cycle Analysis Model called the Greenhouse gases, Regulated Emissions, and Energy use in Transportation (GREET)¹ developed by Argonne National Laboratory forms the core basis of the methodology used in this document. The model however, was modified by TIAX under contract to the California Energy Commission during the AB 1007 process². Using this model, staff developed a pathway document for compressed natural gas (CNG) from Landfill Gas (Bio-Methane) which was made available in mid-2008 on the Low Carbon Fuel Standard (LCFS) website (<http://www.arb.ca.gov/fuels/lcfs/lcfs.htm>). Subsequent to this, the Argonne Model was updated in September 2008. To reflect the update and to incorporate other changes, staff contracted with Life Cycle Associates to update the CA-GREET model. This updated California modified GREET model (v1.8b) (released February 2009)³ forms the basis of this document. It has been used to calculate the energy use and greenhouse gas (GHG) emissions generated during the process of producing and using compressed natural gas (CNG) from Landfill Gas in an internal combustion engine. Landfill gas to CNG pathway is not available in the original Argonne GREET model but has been coded into the CA-GREET model.

The pathway includes landfill gas recovery and pipeline transport to the processing plant where it is upgraded to pipeline quality natural gas and compressed to pipeline pressures. The “natural gas” flows is transported by pipeline to a CNG refueling station where it is compressed and provided to internal combustion vehicles. The values, assumptions, and equations used in this document are from the CA modified GREET model. Figure 1 shows the discrete components that form the CNG from LFG pathway.

This document presents all assumptions, and step by step calculations of energy consumption and GHG emissions for this CNG pathway. Several general descriptions and clarification of terminology used throughout this document are:

- GREET employs a recursive methodology to calculate energy consumption and emissions. To calculate WTT energy and emissions, the values being calculated are often utilized in the calculation. For example, crude oil is used as a process fuel to recover crude oil. The total crude oil recovery energy consumption includes the direct crude oil consumption AND the energy associated with crude recovery (which is the value being calculated).
- Btu/mmBtu is the energy input necessary in Btu to produce or transport one million Btu of a finished (or intermediate) product. This description is used consistently in GREET for all energy calculations. There are 1,055 MJ in one mmBtu of energy.

- gCO₂e/MJ provides the total greenhouse gas emissions on a CO₂ equivalent basis per unit of energy (MJ) for a given fuel. Methane (CH₄) and nitrous oxide (N₂O) are converted to a CO₂ equivalent basis using IPCC global warming potential values and are included in the total.
- GREET assumes that VOC and CO are converted to CO₂ in the atmosphere and includes these pollutants in the total CO₂ value using ratios of the appropriate molecular weights.
- Process Efficiency for any step in GREET is defined as:

$$\text{Efficiency} = \text{energy output} / (\text{energy output} + \text{energy consumed})$$

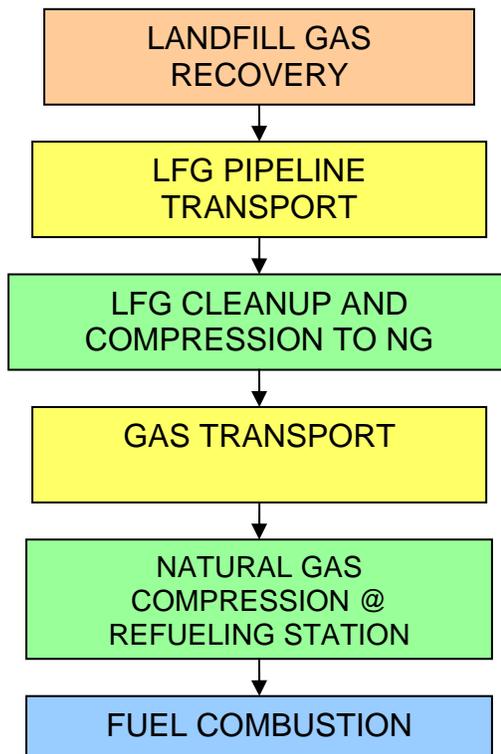


Figure 1. Discrete Components of the Landfill Gas to CNG Pathway

Table A below provides a summary of the results for this LFG to CNG pathway. The WTW analysis shows that **183,840** Btus of energy is required to produce 1 (one) mmBtu of available fuel energy. From a GHG perspective, **11.26** gCO₂e/MJ of GHG emissions are generated during the production and use of CNG in a passenger vehicle. Note that rounding of values has not been performed in several tables in this document. This is to allow stakeholders executing runs with the GREET model to compare actual output values from the CA-modified model with values in this document.

Table A. Summary of Energy Consumption and GHG Emissions per mmBtu of CNG Produced from LFG

	Energy Required (Btu/mmBtu)	GHG Emissions (gCO₂e/MJ)
Landfill Gas Recovery and Transport	9,262	0.49
Landfill Gas Processing	-867,520*	-49.56*
Transport & Distribution	1,350	0.450
Compression at Station	40,748	2.15
Total WTT	-816,160	-46.47
Carbon in Fuel	1,000,000	55.20
Vehicle CH ₄ and N ₂ O		2.53
Total TTW	1,000,000	57.73
Total WTW	183,840	11.26

*Credit for landfill gas processing

The following sections provide summaries of the WTT components as well as the TTW values. Expanded details are provided in Appendix A. A table of all input values is provided in Appendix B.

Landfill Gas Recovery

Tables B and C provide a summary of the energy consumption and associated GHG emissions from LFG recovery and transport. Calculation details are provided in Appendix A.

Table B. Total Energy Consumption by Fuel Type for LFG Recovery and Transport

Fuel Type	Btu/mmBtu
Electricity	9,262
Total	9,262

Table C. Total GHG Emissions from LFG Recovery

	Total GHG gCO₂e/MJ
LFG Recovery	0.49
Total GHG Emissions	0.49

Landfill Gas Processing

Tables D and E provide the energy consumption and associated GHG emissions from LFG processing. Calculation details are provided in Appendix A.

Table D. Total Energy Consumption for the LFG Processing Step

Fuel Type	Btu/mmBtu
Landfill Gas	144,833.1
Electricity	131,151.2
Avoided Flaring Credit	-1,143,504
Total Energy	-867,520

See table 2.02

Table E. Total GHG Emissions from LFG Processing

	Total GHG (gCO ₂ e/MJ)
Landfill Gas	8.431
Electricity	6.878
Flaring Credit	-64.650
Total	-49.56

Natural Gas Transport

Tables F and G summarize energy consumption and GHG emissions from natural gas transport. Calculation details are provided in Appendix A.

Table F. Energy Use for NG Transport

Total T&D Energy Use = 1,350 Btu/mmBtu

See table 3.01

Table G. GHG Emissions from Natural Gas Transport to Refueling Station

	Total GHG gCO ₂ e/MJ
Total	0.45

Natural Gas Compression

Tables H and I provide a summary of energy consumption and GHG emissions from natural gas compression at the refueling station. Calculation details are provided in Appendix A.

Table H. Energy Use for NG Compression, Btu/mmBtu

Total energy use for compression is 40,748 Btu/mmBtu

Table I. Total GHG Emissions Associated with Natural Gas Compression

	CO₂ g/mmBtu	CH₄ g/mmBtu	N₂O g/mmBtu	Total GHG gCO₂e/mmBtu	Total GHG gCO₂e/MJ
Total	2,136	4.5	0.05	2,264	2.15

Natural Gas Tank to Wheel

Table K provides details of WTT GHG emissions from combusting NG in a heavy duty vehicle. Details of calculations are provided in Appendix A.

Table K. Tank to Wheel GHG Emissions for NG

TTW = Vehicle = 57.73g CO₂e/MJ
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APPENDIX A

SECTION 1. LANDFILL GAS RECOVERY AND TRANSPORT

1.1 Energy Use for Landfill Gas Recovery and Transport to Processing

The first step in the CNG from LFG pathway is LFG recovery and transport to the point of processing. Because the location of processing is typically very close to the landfill and the energy consumed in this transport is very small, these two steps are combined into one.

1.1.1 Energy Use for Landfill Gas Recovery

There are three key assumptions made to calculate direct energy consumption for landfill gas recovery:

- Direct Energy Required (4,621.25 Btu/mmBtu, TIAX Estimate¹)
- Fuel Shares (split of total energy consumed by fuel type)
- Leak Rate (0%, TIAX Estimate²)

To recover the LFG, a hermetically sealed electric blower is utilized. The assumed energy required to recover 1 mmBtu of LFG is 4621.25 Btu. Because the blower is hermetically sealed and the landfill cap is under negative pressure, it is assumed that no LFG leaks during the recovery process.

The figure of 4621.25 Btu/mmBtu is the direct energy consumption for the LFG recovery step. This is not the total energy required however, since GREET accounts for the “upstream” energy associated with each of the fuels utilized. The total energy associated with the 4,621.25 Btu of electricity includes the energy used to produce the electricity and the energy used to recover and deliver the fuels to the power plants.

1.1.2 Energy Use for Landfill Gas Transport to Processing

Once the LFG has been recovered, it is transferred a short distance by pipeline to the processing plant. For this pathway it has been assumed that the processing plant is 1 mile from the landfill. For landfill gas transport, hermetically sealed blowers are utilized, so the leak rate is assumed to be zero. The pipeline energy consumption is the energy associated with moving the landfill gas through the pipeline. The main assumptions are:

- Fuel Shares (100% electricity)
- Energy Intensity (203 Btu/ton-mile, calculated from CA-GREET defaults and LFG density)
- Distance (1 mile)

¹ Based on data provided by Prometheus-Energy for the Bowerman landfill in Orange County, California. 37.5 hp are required to recover 770 scfm LFG with an LHV of 446 Btu/scf.

² Standard practice for many years is to use hermetically sealed blowers to transfer landfill and digester gases. Verbal information from Bruce at Spencer Turbine Company (1-800-232-4321) 7/08.

- Lower Heating Value (446 Btu/scf³)
- Density (34.54 g/scf)

The transport pipeline direct energy consumption is calculated as follows:

$$\begin{aligned} \text{Pipeline Energy (Btu/mmBtu)} &= ((34.54 \text{ grams/scf}) / (446 \text{ Btu/scf})) * (1 \text{ mile}) \\ &* (203 \text{ Btu/ton-mile}) * (1 \text{ pound}/454 \text{ grams}) * (1 \text{ ton}/2,000 \text{ pound}) * 1,000,000 \text{ Btu/mmBtu} \\ &= 17.31 \text{ Btu/mmBtu} \end{aligned}$$

1.1.3 Total Direct Energy Consumption and Efficiency for Landfill Gas Recovery and Transport

The total direct energy consumption for LFG recovery and transport of one mile to processing is **4,638.56** Btu/mmBtu. The relationship between figure and the combined recovery and transport efficiency is shown in Table 1.01.

Table 1.01 Calculation of Direct Energy Consumption (Btu/mmBtu) to Recover and Transport LFG from Assumed Values for Recovery Energy and Fuel Shares

Process Fuel Type	Fuel Shares	Relationship of Recovery Efficiency (0.9954) and Fuel Shares	Direct Energy Consumption, Btu/mmBtu
Electricity	100%	$(10^6)(1/0.9954 - 1) * 100\%$	4,638.56
Total Direct Energy Consumption for LFG recovery and transport			4,638.56

Table 1.02 details how total energy is calculated from direct energy shown in Table 1.01. Table 1.03 provides values for factors used in Table 1.02.

³ LHV and density calculated from average fuel properties at Bowerman Landfill, provided by Prometheus-Energy

Table 1.02 Total Energy Consumption from Direct Energy Consumption for LFG Recovery and Transport

Fuel Type	Formula	Btu/mmBtu
Electricity	$A (B + C) / 10^6$	9,262
Total energy for LFG recovery		9,262

Table 1.03 Values Used in Table 1.02

Fuel Type	Description
A	4,638.56 Btu of direct electricity used to recover and transport 1 mmBtu LFG one mile. (see Table 1.01)
B	111,649 Btu of energy used to recover and transport sufficient feedstock to generate 1 mmBtu electricity.
C	1,884,989 Btu used to produce 1 mmBtu electricity.

1.2 GHG Emissions from Landfill Gas Recovery and Transport to Processing

The emission calculation methodology is analogous to the energy calculations. First the direct emissions are calculated and then the upstream emissions (due to recovery and processing of each direct fuel used) are added. To calculate the direct emissions, direct energy by fuel type (provided in detail above) is multiplied by the technology share (% fired in turbine, boiler, engine etc) and then multiplied by the appropriate emission factor. Emissions of CO₂, N₂O and methane due to combustion are quantified. In addition, emissions of VOC and CO are quantified and assumed to convert to CO₂ in the atmosphere. The conversions are calculated as follows:

$$\text{CO (g/MMBtu)} * 44 \text{ gCO}_2/\text{gmole} / 28 \text{ gCO/gmole}$$

$$\text{VOC (g/MMBtu)} * 44 \text{ gCO}_2/\text{gmole} / 12 \text{ gC/gmole} * 0.85 \text{ gC/ gVOC}$$

For LFG recovery and transport, only electric blowers are utilized. Therefore, there are no direct emissions, only upstream emissions from electricity production. The emissions are calculated as follows:

$$\text{Emissions} = \text{Miles} * \text{Energy Intensity} * \text{Fuel Density} / \text{Lower Heating Value} * \text{Upstream Emission Factor}$$

Table 1.04 provides all of the emission factors for electricity production utilized to calculate LFG recovery and transport GHG emissions.

Table 1.04 Emission Factors for California Marginal Stationary Electricity Use, g/mmBtu

	VOC	CO	CH₄	N₂O	CO₂
Feedstock	10.201	18.484	212.375	0.105	8,281
Electricity Generation	5.67	39.677	7.043	2.48	96,250
Total	15.87	58.16	219.42	2.585	104,531

The upstream emissions are those associated with electricity production and electricity feedstock recovery and transport. This pathway utilizes marginal electricity (natural gas and renewables).

Table 1.05 provides the upstream CO₂ emissions for landfill gas recovery and transport. Table 1.06 details the values used in Table 1.04. The total emissions are presented in Table 1.07 along with the other GHGs; the CO and VOC values are converted to CO₂.

Table 1.05 Calculation of Upstream CO₂ Emissions from Direct Energy Consumption for LFG Recovery and Transport

Fuel Type	Formula	g/mmBtu
Electricity	$A (B + C) / 10^6$	485

Table 1.06 Values Used to Calculate Upstream CO₂ Emissions for LFG Recovery

Fuel Type	Description
A	4,638.56 Btu of direct electricity used to recover 1 mmBtu LFG.
B	8,281 g/mmBtu CO ₂ to produce & transport feedstock.
C	96,250 gCO ₂ to produce 1 mmBtu electricity.

Table 1.07 Total GHG Emissions from Landfill Gas Recovery, g/mmBtu

	VOC	CO	CH₄	N₂O	CO₂	CO₂*	Total GHG gCO₂e/mmBtu	Total GHG gCO₂e/MJ
Electricity	0.074	0.270	1.018	0.012	484.8	485.5	514.5	0.488
Total	0.074	0.270	1.018	0.012	484.8	485.5	514.5	0.49

* Includes contributions from VOC and CO.

SECTION 2. LANDFILL GAS PROCESSING

2.1 Energy Use for Landfill Gas Processing

The next step in the LFG to CNG pathway is cleaning the LFG to pipeline quality and compressing it to natural gas distribution pipeline pressures. The LFG processing data are based on an LFG to pipeline facility in Canada⁴. The facility draws 2,570 mmBtu/day of LFG from the landfill (~3,500 scfm) and requires 1.8 MW of grid electricity to run the compressors before the membrane to clean the gas. Currently the facility uses UOP membranes which can achieve 84% methane removal, but the new standard is the Air Liquide MEDAL membrane that can achieve 90% removal efficiency. The Air Liquide MEDAL membrane's 90% removal efficiency⁴ is used in this calculation. The remaining 10% is combusted in a thermal oxidizer to minimize emissions. The thermal oxidizer uses pre-membrane LFG as the fuel at a rate of 3 mmBtu/hr (72 mmBtu/day).

With 2,570 mmBtu/day drawn from the landfill and 72 being used as fuel in the thermal oxidizer, 2,498 mmBtu/day is fed to the membrane where 90% (2,248 MMBtu/day) is sent to the pipeline. The remaining 10% (250 mmBtu/day) is sent to the thermal oxidizer. 1.8 MW (147.41 mmBtu/day) is used as the process energy. Therefore, the overall efficiency of the LFG gas cleaning process is $2,248/(2570+147.41) = 82.7\%$. The breakdown of the process energy used is 322 mmBtu/day total in the thermal oxidizer and 147.41 mmBtu/day from electricity, which is 68.6% and 31.4% respectively

The methodology to calculate direct and total energy for landfill gas processing is the same as that to calculate direct and total energy for LFG recovery. Table 2.01 provides details of direct energy consumption to process landfill gas. Note that this pathway includes a credit for the energy associated with all of the LFG that would have otherwise been flared.

Table 2.01 Calculation of Direct Energy Consumption for LFG Processing

Process Fuel Type	Fuel Shares	Relationship of Process Efficiency (0.827) and Fuel Shares	Direct Energy Consumption, Btu/mmBtu
Landfill Gas	68.6%	$(10^6)/(1/0.827 - 1)(0.686)$	143,504
Electricity	31.4%	$(10^6)/(1/0.827 - 1)(0.314)$	65,686
Flaring Credit		$-(1,000,000 + 143,504)$	- 1,143,504
Direct Energy Consumption for LFG Processing			- 934,314

The values provided in Table 2.01 are direct energy consumption per Btu for the LFG processing step. This is not the total energy required however, since GREET accounts for the "upstream" energy associated with each of the fuels utilized to process the LFG. Table 2.02 demonstrates how the direct energy consumption values shown in Table 2.01 and values in Table 2.03 are utilized to calculate total energy required.

⁴ Emails and conversations between Renewable Solutions Group LLC, Pittsburgh, PA and TIAX LLC.

Table 2.02 Total Energy Consumption from Direct Energy Consumption for LFG Processing

Fuel Type	Formula	Btu/mmBtu
Landfill Gas	$A(1 + B/10^6) * L1$	144,833.1
Electricity	$C (D + E) / 10^6$	131,151.2
Flaring Credit	G	-1,143,504
Total Energy Consumption for NG Processing		- 867,520

Table 2.03 Values Used in Table 2.02

Fuel Type	Description
A	143,504 Btu of direct LFG fuel used per mmBtu LFG processed.
B	Total energy to recover LFG is 9,262 Btu/mmBtu.
C	65,686 Btu of direct electricity used to process 1 mmBtu LFG.
D	111,649 Btu of energy used to recover and transport sufficient feedstock to generate 1 mmBtu electricity.
E	1,884,989 Btu used to produce 1 mmBtu electricity.
L1	Loss factor for LFG transport to processing, 1.000 calculated based on assumption of no leakage.

2.2 GHG Emissions from LFG Processing

As mentioned above, the only fuel directly combusted is LFG in a thermal oxidizer. A large industrial boiler has been used as a surrogate for the thermal oxidizer in GREET when calculating emissions. The exception is the CO₂ emission factor – LFG fuel properties were utilized for this emission factor. Because the LFG would otherwise have been flared, a credit is applied for the flare emissions. The emission factors are provided in Table 2.04. Note that LFG contains approximately 42% CO₂. Two emission factors are shown: the total CO₂ emitted and the CO₂ emitted due to the LFG methane. The emission factor utilized in the calculations is the one that only considers the methane content, since the CO₂ would have been emitted regardless.

Table 2.04 Direct LFG Emission Factors, g/mmBtu

	Large Boiler	Flare
VOC	1.1557	2.5
CO	16.419	26.
CH ₄	1.100	49.
N ₂ O	0.315	1.1
CO ₂ (all LFG Carbon)	107,690	107,523
CO ₂ (only LFG Methane)	58,198	58,048

These emission factors are combined with direct energy consumption to yield direct emissions,. Similar to total energy, the total emissions include direct emissions plus the emissions associated with recovery and processing/refining the fuels used to process landfill gas. Table 2.05 provides the total emissions associated with LFG processing.

Table 2.05 Total Direct and Upstream GHG Emissions for LFG Processing, g/mmBtu

	VOC	CO	CH₄	N₂O	CO₂	CO₂*	Total GHG gCO₂e/ mmBtu	Total GHG gCO₂e/ MJ
Landfill Gas	0.154	3.483	16.257	0.217	8,418	8,424	8,896	8.431
Electricity	1.042	3.820	4.033	0.170	6,866	6,875	7,027	6.878
Flare Credit	-2.859	-29.731	-56.032	-1.258	-66,378	-66,434	-68,209	-64.650
Total	-1.662	-22.43	-35.74	-0.87	-51,093	-51,134	-52,287	-49.56

* Includes contribution from VOC and CO.

SECTION 3. NATURAL GAS TRANSPORT & DISTRIBUTION

3.1 Energy Use for NG Transport and Distribution

The fourth step in the CNG from LFG pathway is transport and distribution of the natural gas by pipeline from the processing plant to the CNG refueling station. For this pathway, it is assumed that the refueling station is located 50 miles from the LFG processing plant. The energy consumption for T&D consists of:

- T&D Feedstock Loss
- T&D Pipeline Transport Energy Consumption

The feedstock loss factor is based on the specification of a leak rate along the transmission & distribution pipelines. The GREET default value is 0.15% however in the AB1007 analysis, Southern California Gas Company (SoCal)⁵ gas provided a report documenting unaccounted for gas losses. This report indicates that pipeline leak rates are 0.08%. (871,900 MCF leakage over 1,052,280,216 MCF system throughput). Therefore the loss factor utilized is significantly lower than the GREET default. Because almost all of this loss occurs in the distribution system, the leak rate does not vary with distance. As discussed in the document describing the CNG from North American Natural Gas pathway, this assumption needs further investigation.

The leak rate is calculated as follows:

$$\text{CH}_4 \text{ Leak Rate} = 0.0008 \text{ g CH}_4/\text{gNG} * 20.4 \text{ g}/930 \text{ Btu} * 10^6 \text{ Btu}/\text{mmBtu} \\ = 17.548 \text{ g}/\text{mmBtu}$$

The leak rate is then used to calculate the Loss Factor (1.001) as follows:

$$\text{Loss Factor} = 17.548 \text{ g}/\text{mmBtu} * 930 \text{ Btu} / 20.4 \text{ g} / 10^6 \text{ Btu}/\text{mmBtu} + 1 = 1.0008$$

Finally, the feedstock loss can be calculated:

$$\text{T\&D Feedstock Loss} = (1.0008 - 1) * 10^6 = \mathbf{800} \text{ Btu}/\text{mmBtu}$$

The pipeline energy consumption is the energy associated with moving the natural gas through the pipeline. The main assumptions are:

- Fuel Shares (94% natural gas, 6% electricity)
- Energy Intensity (405 Btu/ton-mile, current GREET default)
- Distance (50 miles, GREET default is 750 miles)
- Heating value (930 Btu/scf)
- Density (20.4 g/scf)

The T&D pipeline energy consumption is calculated as follows:

$$\text{Pipeline Energy (Btu}/\text{mmBtu)} = ((20.4 \text{ grams}/\text{scf}) / (930 \text{ Btu}/\text{scf})) * (50 \text{ miles})$$

* (405 Btu/ton-mile) * (1 pound/454 grams) * (1 ton/2,000 pound)
*(0.94*1.069+0.06*1.9966) * 1,000,000 = **550 Btu/mmBtu**

The values 1.069 and 1.9966 are the upstream energy in Btu/mmBtu for natural gas and electricity, respectively. As illustrated in Table 3.01, the total T&D energy is the sum of the feedstock loss and pipeline energy consumption.

Table 3.01 Energy Use for NG Transport to Refueling Station

Total T&D Energy Use = 800 + 550 = 1,350 Btu/mmBtu

3.2 GHG Emissions from Natural Gas Transport to the Refueling Station

The pipeline transport emissions are composed of methane leaks and emissions associated with moving the natural gas through the pipeline. As discussed in the energy section, an assumed leak fraction dictates CH₄ leakage emissions of 17.548 g/mmBtu.

The pipeline combustion emissions are set by the GREET default energy intensity of 405 Btu/ton-mile and the assumed transport distance of 50 miles. The direct energy use is 550 Btu/mmBtu. The fuel split is 94% natural gas, 6% electricity. Table 3.02 provides the direct energy consumption and equipment shares. Direct emissions are calculated by multiplying the direct energy for each fuel type in Table 3.02 by the emission factors in Table 3.03. Total emissions are shown in Table 3.04.

Table 3.02 NG Transport Direct Energy Consumption (Btu/mmBtu) and Equipment Shares

	Natural Gas
Direct Energy	517
Equipment Shares	
Turbine	55%
Engine	36%
Advanced Engine	9%
Direct Energy	
Turbine	284
Engine	186
Advanced Engine	47

Table 3.03 Emission Factors for NG Fired Equipment, g/mmBtu

	CO₂	VOC	CO	CH₄ (comb.)	N₂O
Turbine	58,044	0.91	77.18	23.15	2.00
Engine	56,013	230.4	379.8	328.4	2.00
Adv Eng	56,725	61.3	331.4	289.0	2.00

Table 3.04 Direct and Upstream Emissions for NG Transport to Refueling, g/mmBtu

	VOC	CO	CH ₄	N ₂ O	CO ₂	CO ₂ *	Total GHG gCO ₂ e/ mmBtu	Total GHG gCO ₂ e/ MJ
Natural Gas	0.044	0.101	0.131	0.001	28.635	28.931	32.501	0.0308
Electricity	0.000	0.002	0.006	0.000	3.069	3.073	3.257	0.0031
Leakage	0.000	0.000	17.548	0.000	0.000	0.000	438.71	0.4158
Total	0.04	0.10	17.69	0.001	31.70	32.00	474.47	0.45

* Includes contribution from VOC and CO

SECTION 4. NATURAL GAS COMPRESSION TO CNG

4.1 CNG Compression Energy Use

The final step in CNG production is compression at the refueling station. The two assumptions for this part of the analysis are:

- Compression Efficiency (98%)
- Compression Fuel (electric)
- Electricity mix is marginal California mix (NG + renewables)

The GREET default value for compression efficiency is 97%. For the AB1007 analysis, Clean Energy Fuels provided data indicating that compressor efficiency in California is 98.00%. Using this:

Direct electricity use = $10^6 * (1/98.000\% - 1) * 100\% = 20,408.14$ Btu/mmBtu

Total electricity use = $20,408.143 * (111,649 + 1,884,989)/10^6 = 40,748$ Btu/mmBtu
(see table 1.03 for energy required for electricity).

The direct and total electricity uses for compression are therefore **20,408** Btu/mmBtu and **40,748** Btu/mmBtu, respectively.

4.2 GHG Emissions from Natural Gas Compression to CNG

As stated above, this pathway assumes that only electric compressors are used to compress the natural gas. The direct energy use is 20,408 Btu/mmBtu CNG (see section 4.1 above). There are no direct emissions from electricity, only upstream emissions. The upstream emissions associated with electricity production are provided in Table 4.01. These emissions are calculated by multiplying direct energy use in NG compression by CO₂ (shown in table 1.04), VOC, CO, CH₄ and N₂O emission factors. Table 5.02 provides final values (CO and VOC converted to CO₂).

Table 4.01 Upstream Emissions From Electricity Production for Compression, g/mmBtu

	CO₂*	VOC	CO	CH₄ (comb.)	N₂O
Total	2,133.26	0.324	1.19	4.48	0.053

* CO₂ calculation: $((20,408 \text{ Btu/MmmBtu}) * (8,281 + 96,250) \text{ g/mmBtu}) / 10^6 = 2,133.26 \text{ CO}_2 \text{ g/mmBtu}$

Where:

CO₂ emission factor of electricity as feedstock is 8,281 g/mmBtu and as fuels is 96,250 g/mmBtu (see table 1.04 CO₂ emission factor)

Table 4.02 Total GHG Emissions Associated with Natural Gas Compression

	CO₂* g/mmBtu	CH₄ g/mmBtu	N₂O g/mmBtu	Total GHG gCO₂e/mmBtu	Total GHG gCO₂e/MJ
Total	2,136.15	4.478	0.053	2,263.82	2.15

*CO₂ includes contribution from VOC and CO.

SECTION 5. GHG EMISSIONS FROM VEHICLE

5.1 GHG Emissions from Vehicles

The vehicle GHG emissions consist of:

- Tailpipe CO₂ (100% of carbon in fuel goes to CO₂)
- Tailpipe N₂O (combustion product)
- Tailpipe CH₄ (product of incomplete combustion, evaporative losses)

The CO₂ may be directly calculated from finished fuel properties as follows:

$$\text{Vehicle CO}_2 \text{ (g/MJ)} = (20.4 \text{ g NG/scf}) * (0.724 \text{ g C/g NG}) * (1/930 \text{ Btu/scf}) \\ * (44 \text{ g CO}_2 / 12 \text{ g C}) * (\text{Btu}/1.055\text{kJ}) * (1000\text{kJ}/\text{MJ}) = \mathbf{55.2 \text{ g/MJ}}$$

Here, 20.4 g/scf is the density of NG (GREET default), 0.724 is the Carbon in NG (CA-GREET default) and the LHV of NG is 930 Btu/scf. 1.055 is a factor to convert from Btu to kJ.

For CH₄ and N₂O emissions, California Climate Action Registry (CCAR)⁵ g/mile values are used. The CCAR emission factors for CH₄ and N₂O for CNG vehicles are both set at 0.0375 g/mi.

Note: CH₄ and N₂O emission factors for tailpipe emissions have been used as place holder since staff is investigating the availability of appropriate tailpipe emissions data for heavy duty CNG vehicles. When available, staff will adjust contributions from tailpipe emissions CH₄ and N₂O appropriately.

(Note: In a study on CNG use in urban buses⁶, calculations for tailpipe CH₄ and N₂O emissions were approximately 2.82 g/MJ, close to the value shown below).

To convert this to a g/MJ basis, we need to assume a vehicle fuel economy. For the AB1007 analysis, CNG vehicles were assumed to have a fuel economy of 4.8 MJ/mi. Using this value, the vehicle emissions are:

$$\text{Vehicle GHG} = 55.2 \text{ gCO}_2/\text{MJ} + (0.0375 \text{ gN}_2\text{O}/\text{mi} * 298 + 0.0375 \text{ gCH}_4/\text{mi} * 25)/4.8 \\ \text{MJ/mi} = 55.2 + 2.53 = 57.73 \text{ gCO}_2\text{e}/\text{MJ}$$

⁵ <http://www.climateregistry.org/PROTOCOLS/>

⁶ http://www.cleanairnet.org/infopool/1411/articles-59987_resource_1.pdf

APPENDIX B

Compressed Natural Gas from Landfill Gas Pathway Input Values

Parameters	Units	Values	Note
GHG Equivalent			
CO ₂		1	GREET Default
CH ₄		23	GREET Default
N ₂ O		296	GREET Default
VOC		3.1	GREET Default
CO		1.6	GREET Default
Landfill Gas Recovery			
Process Efficiency		99.5%	TIAX Calculation from Data Supplied by Prometheus-Energy
Natural Gas Leak Rate		0%	TIAX Assumption, Communication with Spencer Turbine Company.
Fuel Shares			
<i>Residual Oil</i>		0%	GREET Default
<i>Conventional Diesel</i>		0%	GREET Default
<i>Conventional Gasoline</i>		0%	GREET Default
<i>Natural Gas</i>		0%	GREET Default
<i>Electricity</i>		100%	TIAX Assumption
<i>Feed Loss (Leak)</i>		0%	Calculated from Leak Rate Assumption
Landfill Gas Processing			
Process Efficiency		82.7%	TIAX Calculation from data provided by Renewable Solutions Group LLC for their facility in Canada
Natural Gas Leak Rate		0 %	TIAX Assumption based on email exchange with Prometheus-Energy
Fuel Shares			
<i>Natural Gas</i>		68.6%	TIAX Calculation from data provided by Renewable Solutions Group LLC
<i>Electricity</i>		31.4%	TIAX Calculation from data provided by Renewable Solutions Group LLC
Equipment Shares			
<i>CO₂ Emission Factor</i>	gCO ₂ /mmBtu	58,054	TIAX calculation for avg LFG at Bowerman landfill in Southern California. Only includes CO ₂ produced by combusting the CH ₄ , not the CO ₂ present in LFG since this would be emitted anyway.
<i>Large Boiler - NG</i>		100%	TIAX Assumption
CNG Compression			
Efficiency		98.0%	Based on Data Provided by Clean Energy Fuels
Process Shares			
<i>Electricity</i>		100%	AB 1007 Assumption
CNG Transportation and Distribution			
Leak Rate		0.08%	Based on Data Provided by SoCal Gas Ab1007
Transportation by pipeline		100%	GREET Default
<i>Distance</i>	miles	50	TIAX Assumption
<i>Energy Intensity</i>	Btu/ton-mile	344	GREET Default
Fuel Shares			
<i>Natural Gas</i>		94%	GREET Default
<i>Electricity</i>		6%	GREET Default
Equipment Shares			
<i>Turbine - NG</i>		55%	GREET Default
<i>CO₂ Emission Factor</i>	gCO ₂ /mmBtu	58,196	GREET Default
<i>Engine - NG</i>		36%	GREET Default
<i>CO₂ Emission Factor</i>	gCO ₂ /mmBtu	56,013	GREET Default
<i>Advanced Engine - NG</i>		9%	GREET Default

Parameters	Units	Values	Note
<i>CO₂ Emission Factor</i>	gCO ₂ /mmBtu	56,388	GREET Default
Loss Factor of CNG by T&D		1.00122	GREET Default
Fuels Specifications	LHV (Btu/gal)	Density (g/gal)	
<i>Crude</i>	129,670	3,205	GREET Default
<i>Residual Oil</i>	140,353	3,752	GREET Default
<i>Conventional Diesel</i>	128,450	3,167	GREET Default
<i>Conventional Gasoline</i>	116,090	2,819	GREET Default
<i>Natural Gas</i>	83,686	2,651	as liquid - for gaseous LHV: 930 Btu/SCF, 20.4 g/SCF
<i>Landfill Gas</i>	446 Btu/scf	34.54 g/scf	TIAX calculation from avg fuel composition at Bowerman Landfill in Southern California

¹ GREET Model: Argonne National Laboratory:
http://www.transportation.anl.gov/modeling_simulation/GREET/index.html

² California Assembly Bill AB 1007 Study: <http://www.energy.ca.gov/ab1007>

³ CA_GREET Model (modified by Lifecycle Associates) released February 2009
<http://www.arb.ca.gov/fuels/lcfs/lcfs.htm>

⁴ CO₂ Membrane Technology by Air Liquide MEDAL:
<http://www.medal.airliquide.com/en/co-membrane/co-membrane-technology.html>

⁵ "A Study of the 1991 Unaccounted for Gas Volume At the Southern California Gas Company", Aug 1993.